

# Model Predictive Control for Robots in Ocean Waves

As presented by:

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M.S. Candidate

Robotics

#### **About Me**



- 1<sup>st</sup> year in Coastal/Ocean Engineering
- Summer 2014: Hinsdale Wave Research Lab
- Supported CEOAS and OOI glider groups
- 2<sup>nd</sup> year with Robotic Decision Making Lab











#### **Motivation**



- Ocean waves will displace a robot
- Wave disturbances lend to increased sensor drift



Source: National Geographic, 2012, R. D. Ballard

- Sensor drift reduces robotic observation quality
- Impending wave forces can be estimated
- Objective: keep a station-keeping robot stationary under the influence of a wave field

# Motivation

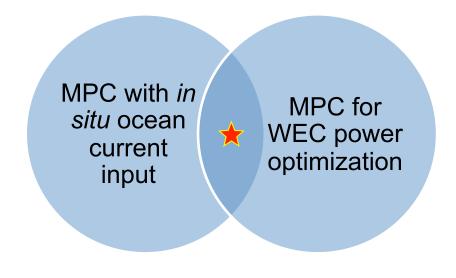




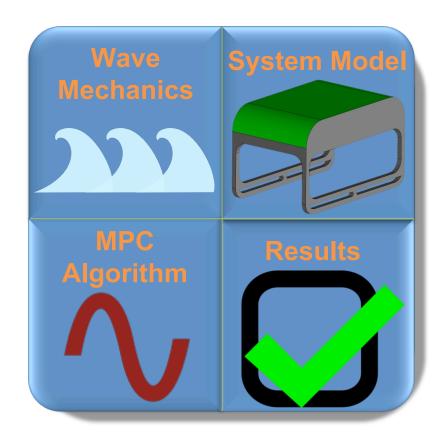
#### **Related Work**

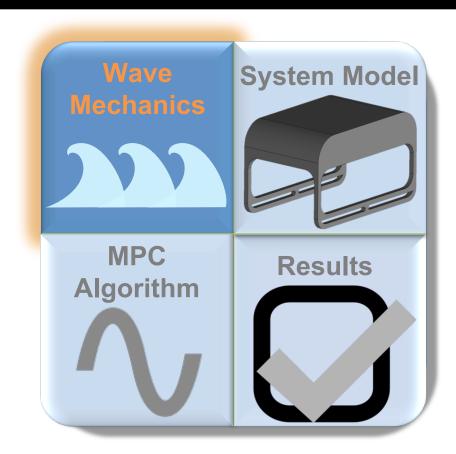


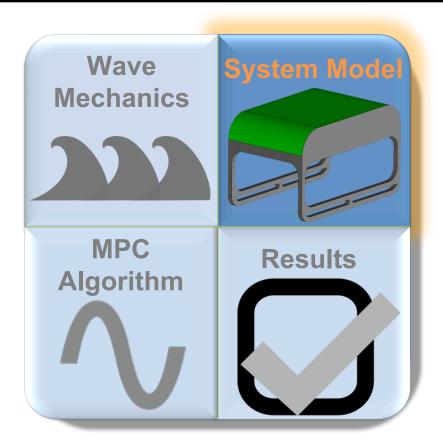
- Model Predictive Control (MPC)
  - Path planning with in situ ocean currents (Medagoda, 2012)
  - Wave Energy Converter (WEC) optimization (Brekken, 2011)

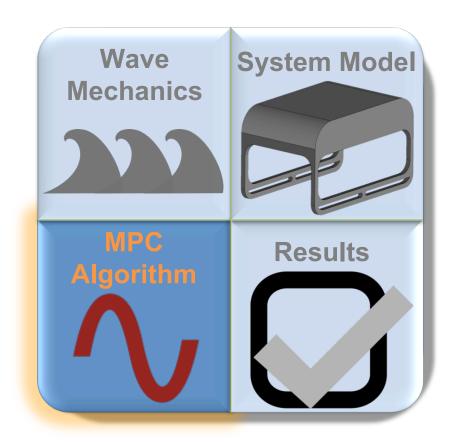


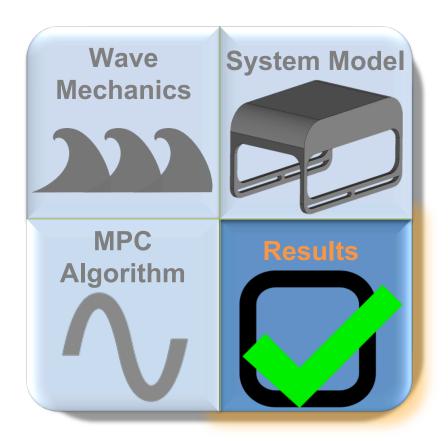
Station-keeping under water waves (Heidel, 1998)

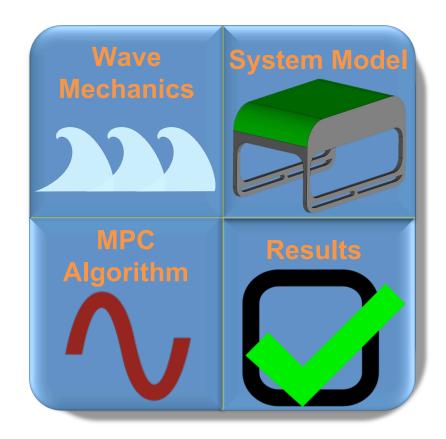


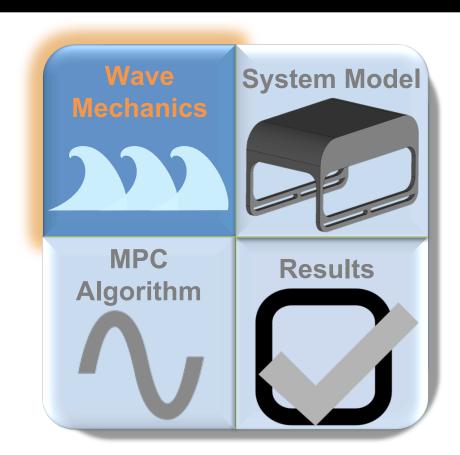


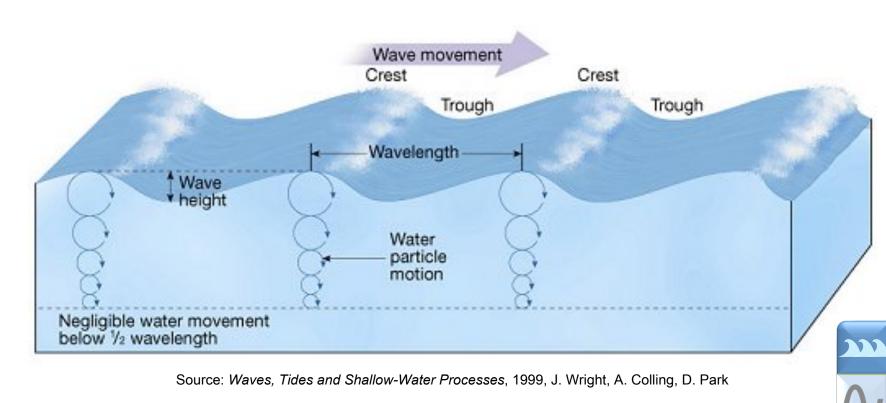






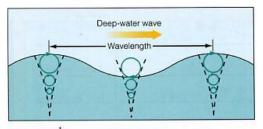


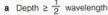


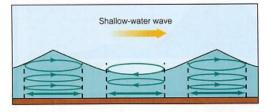


#### Water Motion under Waves

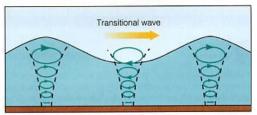








b Depth ≤ 1/20 wavelength



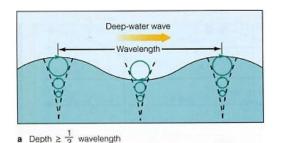
c  $\frac{1}{20}$  wavelength  $\leq$  depth  $\leq$   $\frac{1}{2}$  wavelength

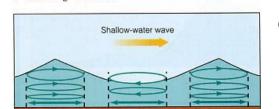
- Deep water wave
  - circular paths, exponential decrease with depth
  - vlp=1/2 at z=-L/9, close to 0 at z=-L/2
- Shallow water wave
  - More lateral motion than vertical
  - More elliptical with depth, virtually lateral at depth
- Transitional water depths
  - Intermediate elliptical patterns
  - Majority of waves in this work



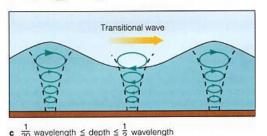
#### Water Motion under Waves







b Depth ≤ ½ wavelength



- Deep water wave
  - circular paths, exponential decrease with depth
  - v l p = 1/2 at z = -L/9, close to 0 at z = -L/2
- Shallow water wave
  - More lateral motion than vertical
  - More elliptical with depth, virtually lateral at depth
- Transitional water depths
  - Intermediate elliptical patterns
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# Simulation Setting (NETS)



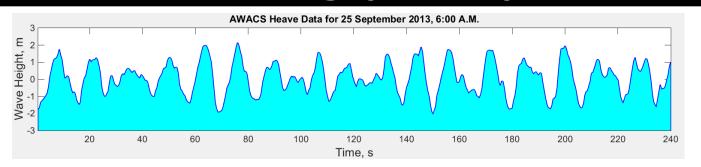
- North Energy Test Site
- Operational depth: 50 m
- Validation of wave field
  - AWAC acoustic measurements
  - Deployed at NETS
  - August October 2013
  - (600) 40 minute profiles (2 Hz)

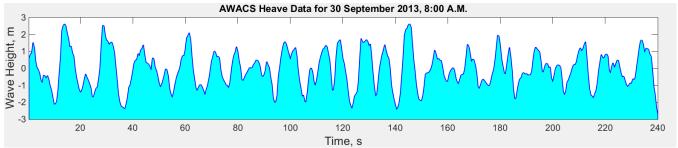


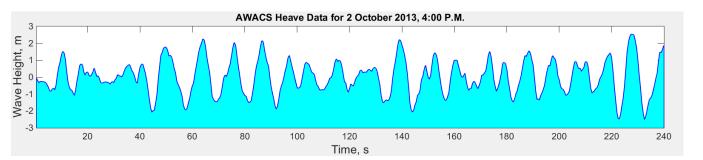


# Simulation Setting (NETS)







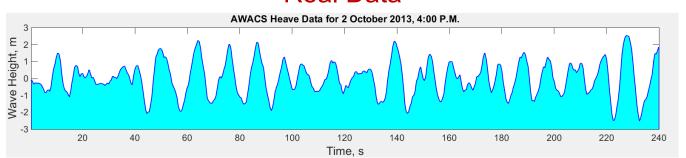




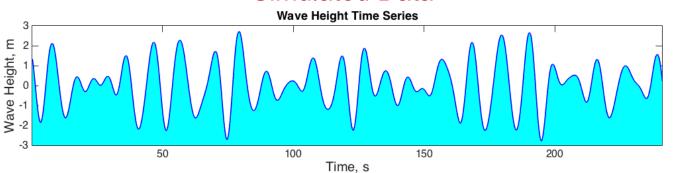
# Simulation Setting (NETS)



#### **Real Data**



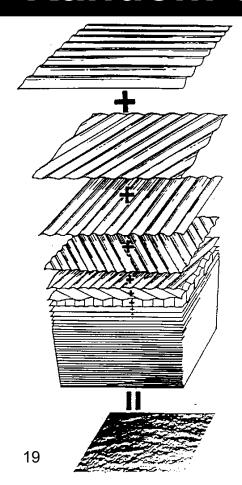
#### Simulated Data





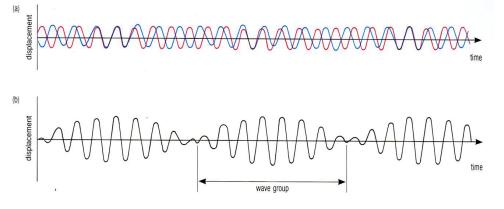
#### **Random Seas**





#### Superposition

 Sea surface can be represented by the sum of sinusoids with component periods (T), amplitudes (a), and phase offsets (φ)

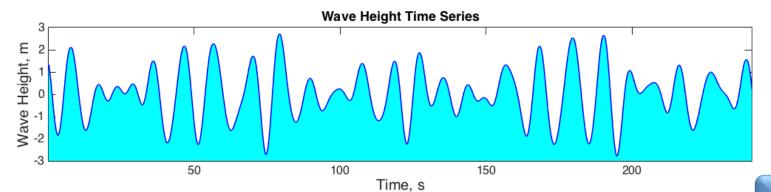




#### Oregon State

# Input Wave Field

Component Wave	1	2	3	4	5	6	7	8
Wave Period, $T$ , s	10	8	12	11	6	7	9	25
Wave Height, $H$ , m	1.8	0.9	1.6	1.3	0.4	0.5	1.1	0.7
Phase, $\phi$ , rad	$-\frac{\pi}{2}$	$-\frac{\pi}{4}$	$-\frac{5\pi}{8}$	$\frac{4\pi}{13}$	$-\frac{\pi}{15}$	$\frac{\pi}{3}$	$-\frac{\pi}{18}$	$-\frac{7\pi}{4}$



$$\eta(\mathbf{t}) = \sum_{k=0}^{\infty} \frac{H}{2} \cos(k\mathbf{x} - \omega \mathbf{t} + \phi)$$

## **Linear Wave Theory**



Assumes potential flow: u=νφ

- Dispersion Relation: ω12 = gktan h(kd)
- Wavelength:  $L=gT12/2\pi \left[\tanh\left((\omega 12\ d/g)13/4\ \right)\right]12/3$
- Wavenumber:  $k=2\pi/L$



#### Water Motion under Waves

#### Lateral motion in transitional water

$$\mathbf{v}_{p,\mathbf{x}} = \frac{HgT}{2L} \frac{\cosh \frac{2\pi(\mathbf{z}+d)}{L}}{\cosh \frac{2\pi d}{L}} \cos(k\mathbf{x} - \omega \mathbf{t} + \phi),$$

$$\dot{\mathbf{v}}_{p,\mathbf{x}} = \frac{g\pi H}{L} \frac{\cosh\frac{2\pi(\mathbf{z}+d)}{L}}{\cosh\frac{2\pi d}{L}} \sin(k\mathbf{x} - \omega\mathbf{t} + \phi).$$



#### Water Motion under Waves

#### Vertical motion in transitional water

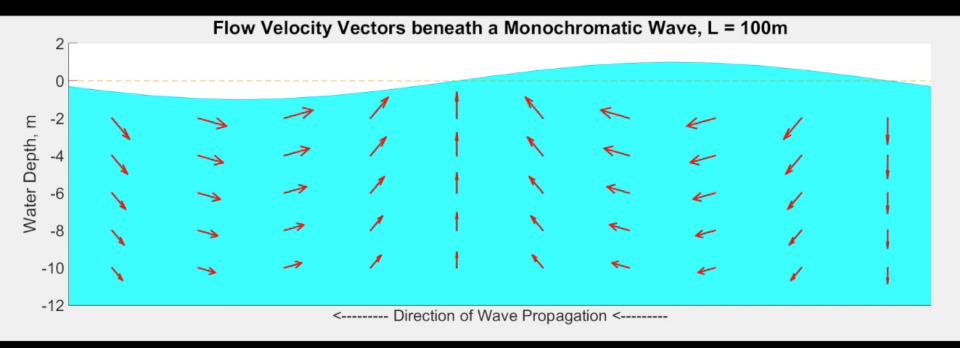
$$\mathbf{v}_{p,\mathbf{z}} = \frac{HgT}{2L} \frac{\sinh \frac{2\pi(\mathbf{z}+d)}{L}}{\cosh \frac{2\pi d}{L}} \sin(k\mathbf{x} - \omega \mathbf{t} + \phi),$$

$$\dot{\mathbf{v}}_{p,\mathbf{z}} = -\frac{g\pi H}{L} \frac{\sinh\frac{2\pi(\mathbf{z}+d)}{L}}{\cosh\frac{2\pi d}{L}} \cos(k\mathbf{x} - \omega\mathbf{t} + \phi).$$

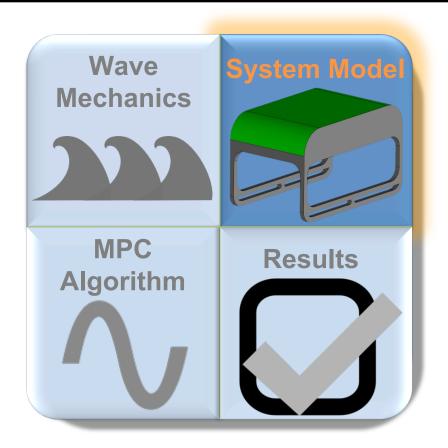


# Simulator (Fluid Motion)









# Remotely Operated Vehicle



#### SeaBotix vLBV300

- Payload: 10kg
- Depth Rating: 300m
- Doppler Velocity Log (DVL)
- Inertial Measurement Unit (IMU)
- (6) 100mm brushless DC thrusters
- Low light color camera with 180° vertical tilt

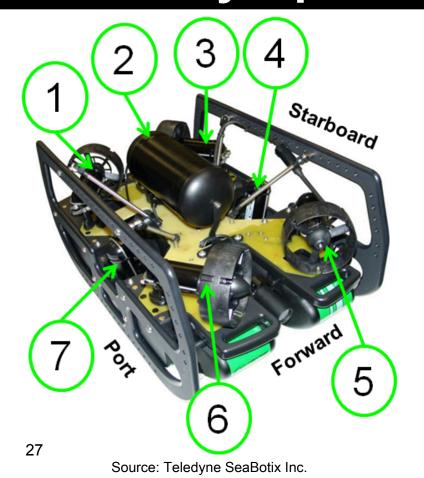


Source: Teledyne SeaBotix Inc.



#### **Remotely Operated Vehicle**



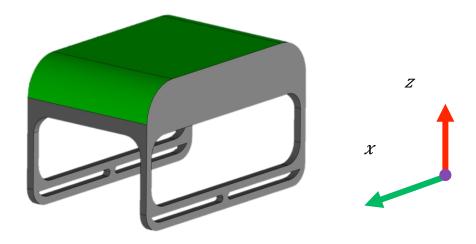


- 1. Port aft thruster
- 2. Electronics tube
- 3. Starboard aft thruster
- 4. Starboard vertical thruster
- 5. Starboard forward thruster
- 6. Port forward thruster
- 7. Port vertical thruster



# Remotely Operated Vehicle

- Dassault SolidWorks
- Ansys AQWA



Parameter	Symbol	Value		
Density of Seawater	$\rho_{sea}$	$1030 \ kg/m^3$		
Incident Area, x	$A_{i,\mathbf{x}}$	$0.156 \ m^2$		
Incident Area, z	$A_{i,\mathbf{z}}$	$0.273 \ m^2$		
Moment of Inertia, x	$I_{xx}$	$0.62~kg~m^2$		
Moment of Inertia, z	$I_{zz}$	$1.60~kg~m^2$		
Dry Mass	$m_{dry}$	22.2~kg		
Added Mass, x	$m_{add,x}$	8.1~kg		
Added Mass, z	$m_{add,z}$	$36.7 \ kg$		
Drag Coefficient, x	$c_{d,x}$	0.84		
Drag Coefficient, z	$c_{d,z}$	1.06		
Max Thruster Force	$T_{max}$	29.7 N		
Thruster Angle, Forward	$\theta_f$	35°		
Thruster Angle, Aft	$\theta_a$	45°		
Thruster Angle, Vertical	$\theta_v$	20°		





System differential equation of motion:

$$\mathbf{M}\dot{\mathbf{v}}_a = \mathbf{F}_{thrust} + \mathbf{F}_d + \mathbf{F}_g + \mathbf{F}_c$$

Simplify, sub inertia and drag relations:

$$m_{dry}\dot{\mathbf{v}}_a + m_{add}\dot{\mathbf{v}}_r = \mathbf{F}_{thrust} + \frac{1}{2}\rho_{sea}A_ic_d|\mathbf{v}_r|\mathbf{v}_r$$





System differential equation of motion:

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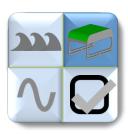




• Substitute  $p_{lp}$  such that  $p_{la} = p_{lr} + p_{lp}$ :

$$\begin{bmatrix} m_{dry} + m_{add,\mathbf{x}} \\ m_{dry} + m_{add,\mathbf{z}} \end{bmatrix} \begin{bmatrix} \ddot{\mathbf{x}} \\ \ddot{\mathbf{z}} \end{bmatrix} = \begin{bmatrix} \mathbf{F}_{thrust,\mathbf{x}} \\ \mathbf{F}_{thrust,\mathbf{z}} \end{bmatrix} + \begin{bmatrix} m_{add,\mathbf{x}} \\ m_{add,\mathbf{z}} \end{bmatrix} \begin{bmatrix} \dot{\mathbf{v}}_{p,\mathbf{x}} \\ \dot{\mathbf{v}}_{p,\mathbf{z}} \end{bmatrix} + \frac{\rho_{sea}}{2} \begin{bmatrix} A_{i,\mathbf{x}}C_{d,\mathbf{x}} \\ A_{i,\mathbf{z}}C_{d,\mathbf{z}} \end{bmatrix} \begin{bmatrix} |\dot{\mathbf{x}} - \mathbf{v}_{p,\mathbf{x}}|(\dot{\mathbf{x}} - \mathbf{v}_{p,\mathbf{x}}) \\ |\dot{\mathbf{z}} - \mathbf{v}_{p,\mathbf{z}}|(\dot{\mathbf{z}} - \mathbf{v}_{p,\mathbf{z}}) \end{bmatrix}$$

• where:  $v \downarrow a, x=x$  and  $v \downarrow a, z=z$ 





In state space form:

$$\dot{\mathbf{\Upsilon}} = \begin{bmatrix} \dot{\mathbf{x}} & \ddot{\mathbf{x}} & \dot{\mathbf{z}} & \ddot{\mathbf{z}} \end{bmatrix}^T = \mathbf{A}\mathbf{\Upsilon} + \mathbf{B}\mathbf{u} + \mathbf{D}$$

• where:  $x = v \downarrow a$ , x and  $z = v \downarrow a$ , z





$$\mathbf{A}\mathbf{\Upsilon} = \begin{bmatrix} 0 & 1 & 0 & 0 & | & \mathbf{x} \\ 0 & 0 & 0 & 0 & | & \dot{\mathbf{x}} \\ 0 & 0 & 0 & 1 & | & \mathbf{z} \\ 0 & 0 & 0 & 0 & | & \dot{\mathbf{z}} \end{bmatrix}$$





		0	0	0	0	0	$\begin{bmatrix} 0 \\ 0 \\ 0 \\ -cos\theta_v \end{bmatrix}$
Bu =	$T_{max}$	$cos\theta_f$	$cos\theta_f$	$-cos\theta_a$	$-cos\theta_a$	0	0
Da	$m_{dry}$	0	0	0	0	0	0
		0	0	0	0	$-cos\theta_v$	$-cos\theta_v$

 $u_1$  $u_2$  $u_3$  $u_4$  $u_5$  $u_6$ 



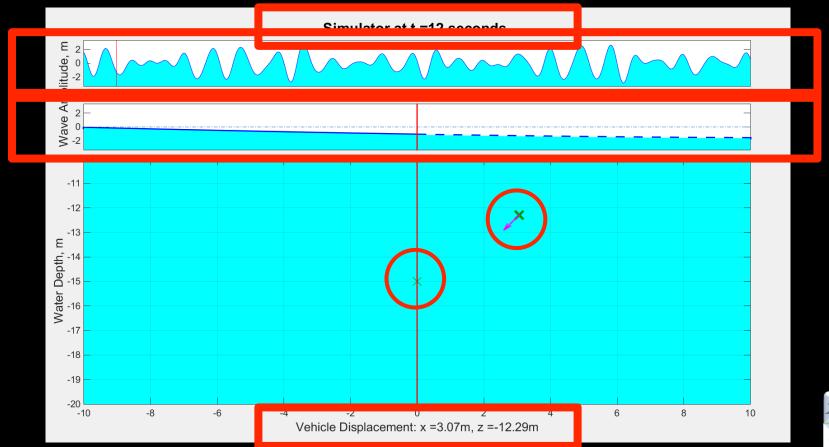


$$\mathbf{D} = \begin{bmatrix} \frac{\dot{\mathbf{v}}_{p,\mathbf{x}}}{m_{dry}} + \frac{\rho_{sea}A_{i,\mathbf{x}}C_{d,\mathbf{x}}}{2(m_{dry} + m_{add,\mathbf{x}})} | \dot{\mathbf{x}} - \mathbf{v}_{p,\mathbf{x}} | (\dot{\mathbf{x}} - \mathbf{v}_{p,\mathbf{x}}) \\ 0 \\ \frac{\dot{\mathbf{v}}_{p,\mathbf{z}}}{m_{dry}} + \frac{\rho_{sea}A_{i,\mathbf{x}}C_{d,\mathbf{z}}}{2(m_{dry} + m_{add,\mathbf{z}})} | \dot{\mathbf{z}} - \mathbf{v}_{p,\mathbf{z}} | (\dot{\mathbf{z}} - \mathbf{v}_{p,\mathbf{z}}) \end{bmatrix}$$



#### **Simulator**

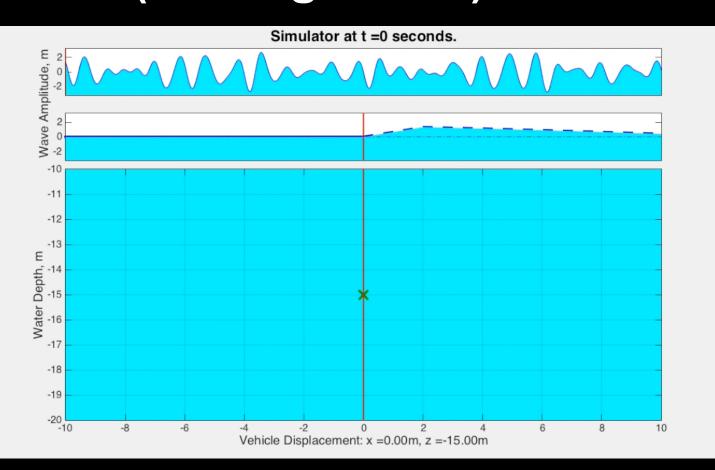






# Simulator (Drifting Robot)







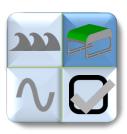
## Feedback Control



Purely Reactive

Use as base of comparison

Position Derivative (PD) control



#### PD Controller



• Positional Error: ε↓P=r↓target-r↓n

• Derivative Error:  $\epsilon \downarrow D = \epsilon \downarrow P, n - \epsilon \downarrow P, (n-1)$ 

- $[u\downarrow 1 \ u\downarrow 2 \ u\downarrow 3 \ u\downarrow 4 \ ]\uparrow T = K\downarrow P, x \in \downarrow P, x + K\downarrow D, x \in \downarrow D, x$
- $[u \downarrow 5 \ u \downarrow 6] \uparrow T = K \downarrow P, \mathbf{z} \in \downarrow P, \mathbf{z} + K \downarrow D, \mathbf{z} \in \downarrow D, \mathbf{z}$



#### **PD Controller**



• Positional Error: ε↓P=r↓target-r↓n

• Derivative Error:  $\epsilon \downarrow D = \epsilon \downarrow P, n - \epsilon \downarrow P, (n-1)$ 

- $[u \downarrow 1 \ u \downarrow 2 \ u \downarrow 3 \ u \downarrow 4 \ ] \uparrow T = K \downarrow P, \boldsymbol{x} \in \downarrow P, \boldsymbol{x} + K \downarrow D, \boldsymbol{x} \in \downarrow D, \boldsymbol{x}$
- $[u\downarrow 5 \ u\downarrow 6]\uparrow T=K\downarrow P, \mathbf{z}\in \downarrow P, \mathbf{z}+K\downarrow D, \mathbf{z}\in \downarrow Q, \mathbf{z}$

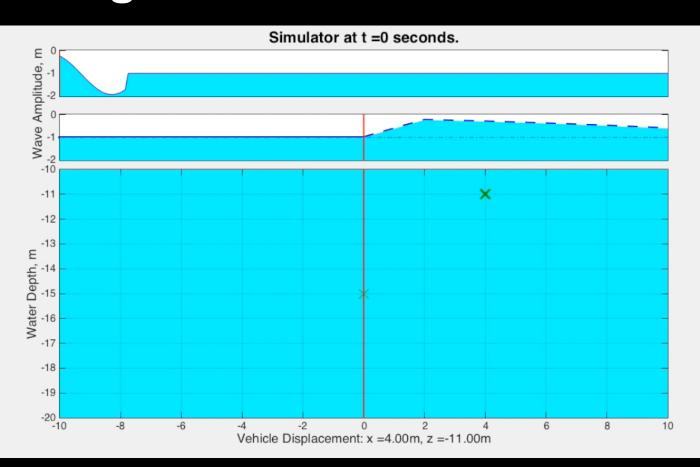






# **PD Tuning**

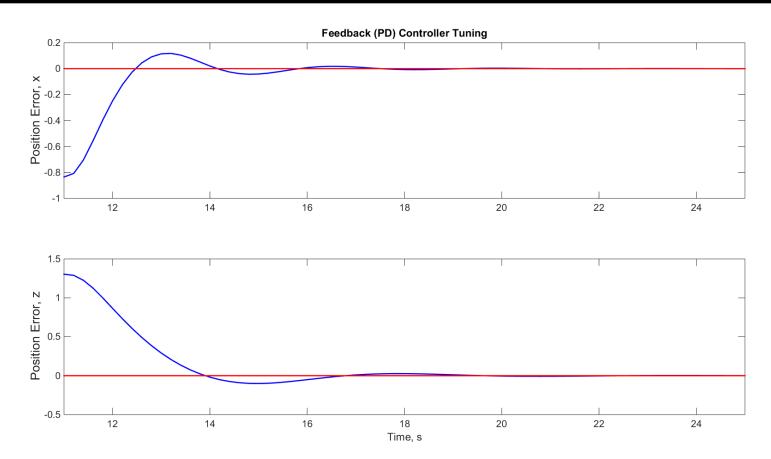






# **PD Tuning**

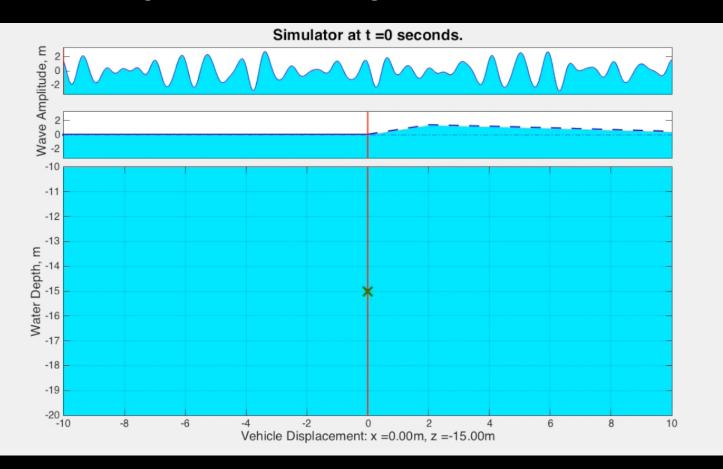






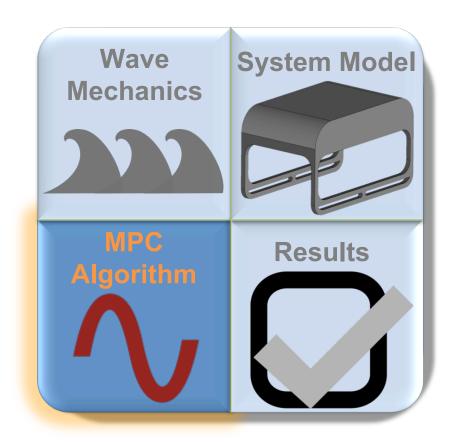
#### Oregon State

## Simulator (PD Robot)





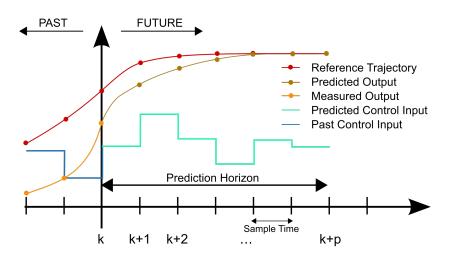
## Outline



#### **Model Predictive Control**



- State estimator
- Cost function
- Receding horizon



 Objective: Find the control actions that minimize the distance between the desired and predicted states.



#### **Cost Function**



$$J = \sum k = 1 \uparrow N = [Y \downarrow target - Y \downarrow k (u \downarrow k)] \uparrow 2 + \beta u \downarrow k \uparrow 2$$

$$u \downarrow 1: N \uparrow * = arg \min_{-u \downarrow 1: N} J(u \downarrow 1: N)$$



## **Gradient Descent Optimization**



- Perturb new control input by Jacobian
  - Minimized as optimal control action is approached

```
\partial J/\partial u = J \ln - J \ln - 1 / u \ln - u \ln - 1
```





- 1: **procedure**  $MPC(t, \lambda, \text{robot}, \Upsilon_{target})$
- $2: n \leftarrow 1$
- 3:  $\eta \leftarrow \text{LOADSEASTATE}(t, \lambda, \Upsilon_{initial})$
- 4: **while** n < simulatorOff do
- 5: input  $\leftarrow$  GETFORECAST( t, robot,  $\lambda$ ,  $\Upsilon_{target}$ , n)
- 6: robot  $\leftarrow$  MOVEROBOT( t, robot,  $\lambda$ , input, n)
- 7:  $n \leftarrow n+1$





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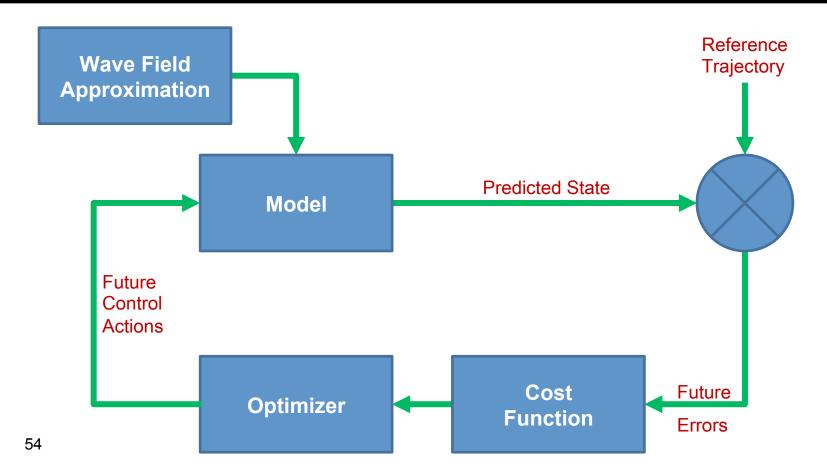
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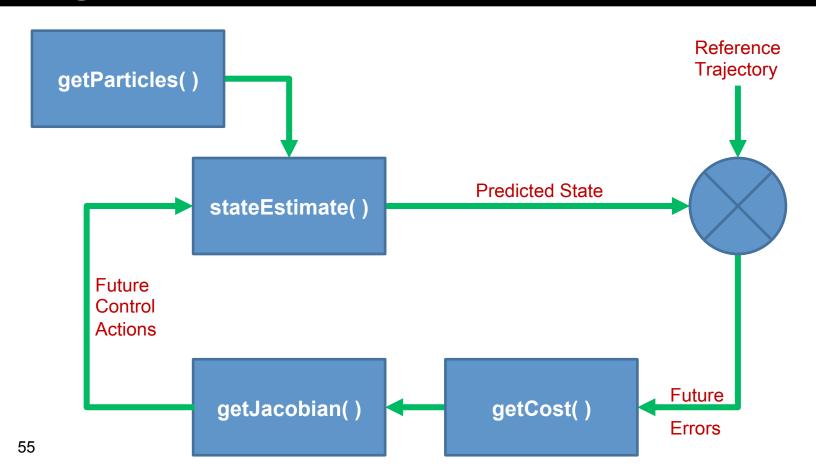


```
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7: n \leftarrow n + 1
```











14:

15:

16:

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2 56



10	1-21- / /	T4 4:	- 2 L	:40-:4:1-
13:	while $i <$	maxIterations	and $0 >$	exitCriteria do

$$u_{i+1} \leftarrow u_i - \delta$$

for 
$$k \in [1, 2, ..., N]$$
 do

or 
$$\kappa \in [1, 2, ..., N]$$
 do

$$\mathbf{v}_p, \dot{\mathbf{v}}_p \leftarrow \text{GETPARTICLES}(t, \Upsilon_i(k), \lambda)$$

$$\mathbf{v}_p, \mathbf{v}_p \leftarrow \text{GETPARTICL}$$

$$\Lambda \leftarrow \mathbf{v}_p, \dot{\mathbf{v}}_p$$

$$\Lambda \leftarrow \mathbf{v}_p, \mathbf{v}_p$$
  
 $\Upsilon_{i+1}(k) \leftarrow \text{STATEESTIMATE}(t, \text{ robot}, \Lambda, u_{n+1}(k))$ 

$$J_{i+1}(k) \leftarrow \text{GETCOST}(\Upsilon_{target}, \Upsilon_{i+1}(k))$$

$$\delta \leftarrow \text{GETJACOBIAN}(J_i, J_{i+1}, u_i, u_{i+1})$$

$$u_i \leftarrow u_{i+1}$$

$$J_i \leftarrow J_{i+1}$$

$$\Upsilon_i \leftarrow \Upsilon_{i+1}$$

24: 
$$i \leftarrow i + 1$$

23: 
$$\Upsilon_i \leftarrow \Upsilon_{i+}$$
  
24:  $i \leftarrow i+1$ 

return  $u_{i+1}$ 



14:

15:

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22:

2 57



13: while $i < \text{maxIterations and } \delta > \text{exitCrit}$	eria do

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**107**  $\kappa \in [1, 2, ..., N]$  **do**

$$\dot{\mathbf{v}} \leftarrow \mathbf{CETPAPTICI}$$

$$\mathbf{v}_p, \dot{\mathbf{v}}_p \leftarrow \text{GETPARTICLES}(t, \Upsilon_i(k), \lambda)$$

$$\Lambda \leftarrow \mathbf{v}_p, \dot{\mathbf{v}}_p$$

$$\Lambda \leftarrow \mathbf{v}_p, \mathbf{v}_p$$

$$\Upsilon_{i+1}(k) \leftarrow \text{STATEESTIMATE}(t, \text{ robot}, \Lambda, u_{n+1}(k))$$
  
 $J_{i+1}(k) \leftarrow \text{GETCOST}(\Upsilon_{target}, \Upsilon_{i+1}(k))$ 

$$\delta \leftarrow \text{GETJACOBIAN}(J_i, J_{i+1}, u_i, u_{i+1})$$

$$u_i \leftarrow u_{i+1}$$

$$J_{i+1}$$

$$J_i \leftarrow J_{i+1}$$

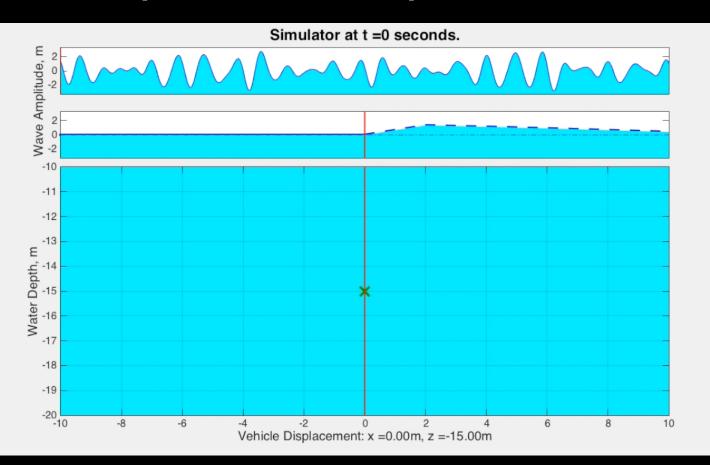
23: 
$$\Upsilon_i \leftarrow \Upsilon_{i+1}$$

24: 
$$i \leftarrow i+1$$
2 57 **return**  $u_{i+1}$ 



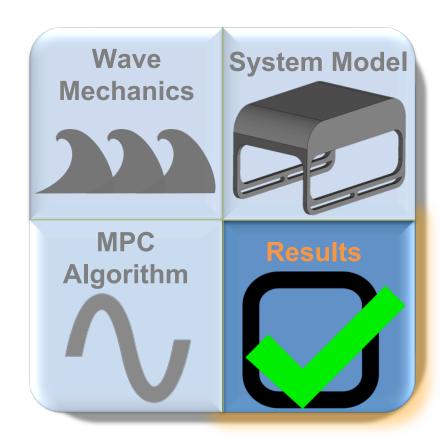
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# Simulator (MPC Robot)





## Outline



#### Results



Determine best performing horizon

MPC performance versus PD control

Resistance to noisy sensor observations



#### **Ideal Horizon**



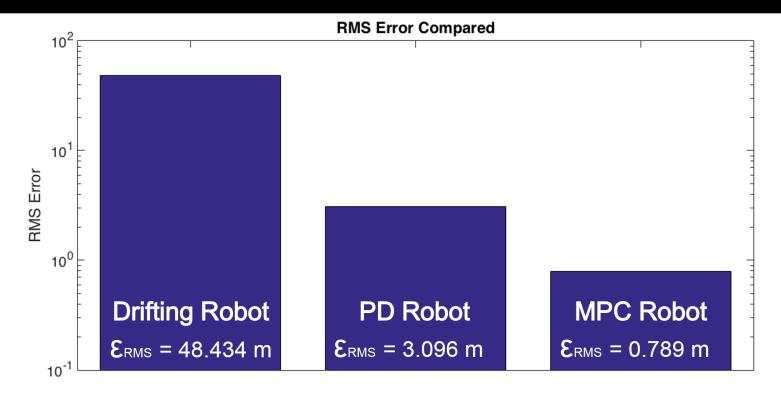
Horizon, s	0.2	0.4	0.8	1.0	1.6	2.0	3.0
$\epsilon_{RMS}$ , m	5.02	2.11	0.79	0.65	0.29	0.05	9.0E-6
$\sum t_{Calc}$ , s	1658	507.1	93.8	233.2	7808	21886	101252
$\bar{t}_{Calc}$ , s	6.90	2.11	0.39	0.97	32.53	91.19	421.88

- 0.8s best balance of low error and time
- Poor performers on low & high end
- Total time: 240s discretized by 0.2s



#### **MPC Performance**



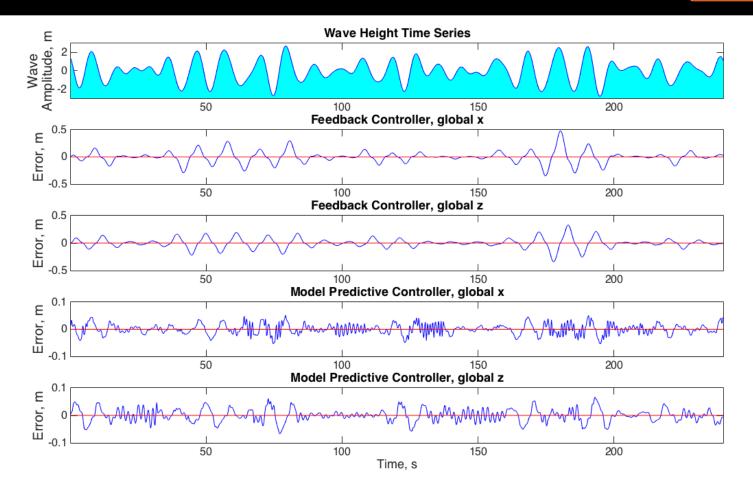


74% reduction in position error over PD



#### **MPC Performance**

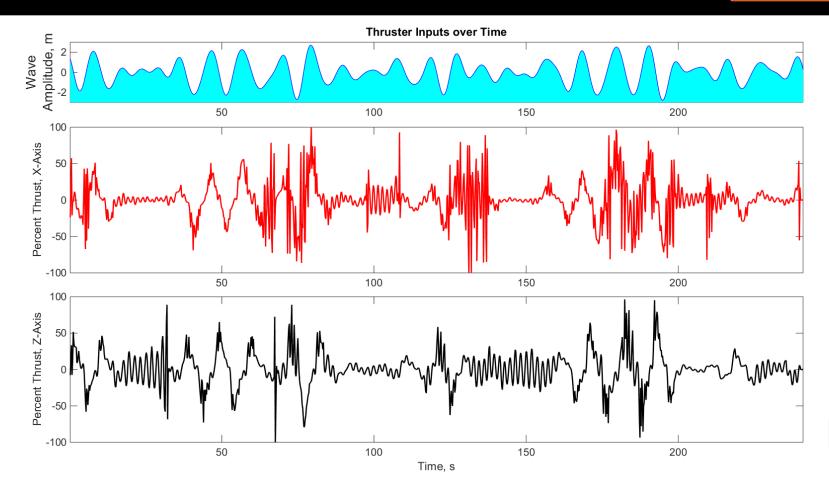






#### **MPC Performance**







### Impact of Gaussian Noise

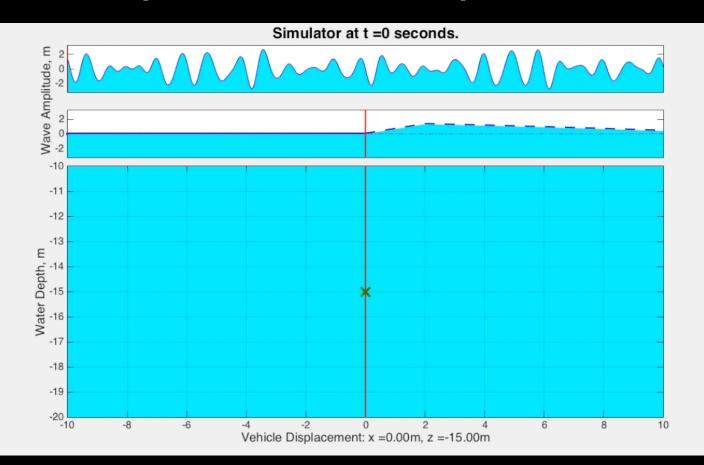


- Observations of perceived wave state
- H term assigned maximum variance
- Minimal localization noise assumed
  - Deterministic PD case



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# Simulator (MPC w/ noise)





### Impact of Gaussian Noise



- 50 simulations
  - getForecast() gets new noisy wave field at n<sup>th</sup> step
- 44% reduction over PD
  - $\epsilon \downarrow RMS = 1.737 m$
  - $\sigma = 0.059$
- Notable run time increase



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## **Summary of Contributions**

- A feedforward control (MPC) method that can forecast and compensate for impending wave forces
- Application of the MPC algorithm to a simulated stationkeeping robot
- Comparison of the MPC algorithm against traditional feedback (PD) control
- Algorithm resistance to noisy sensor observations of wave field parameters.
- Recommendations for choosing a prediction horizon

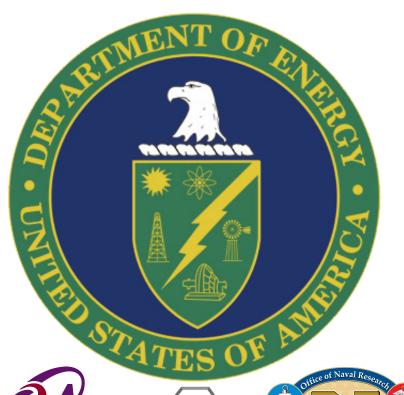
#### **Future Work**



- Real-time wave prediction methods
- Neuro-Evolutionary control methods
  - Hydrodynamic simulation software packages
- System dynamics expanded
- More efficient optimization

## Sponsors and Affiliations







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